



STANFORD

Supplementary Lecture 4C
Wireless Channels

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Announcements & Agenda

- Goals
 - Familiarize, or reacquaint, interested students/researchers to obtain an $H(f)$ for a wireless channel (with antennas)
 - Permit construction of real or complex baseband-equivalent channels for analysis.

This is second of 3 short lectures online

S4A: Transmission Line

S4B: Waveguide

S4C: Wireless (with antennas)

- Topics
 - Filtered AWGN
 - Isotropic and Dipole Antennas
 - Antenna arrays
 - MIMO Beam forming/steering
 - 2D array

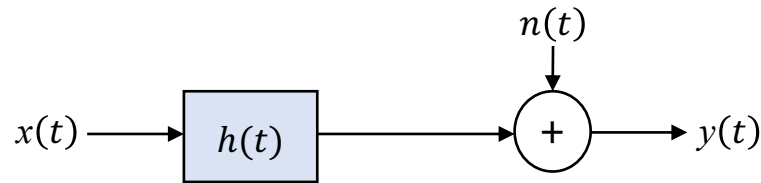


Finding $H(f)$

Section 1.3.8

Computation of $H(f)$

- **Channel filter** $h(t) \leftrightarrow H(f)$ from electromagnetic modelling.

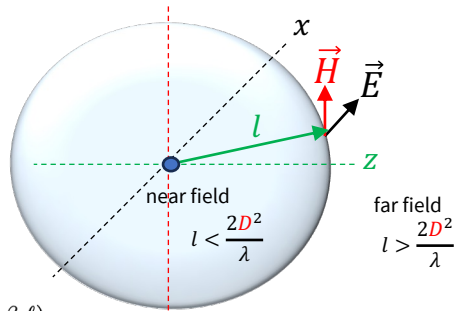


- **Noise:** AWGN often specifies a PSD, like -174 dBm/Hz
 - This is room temperature noise $k \cdot T$ (Boltzman constant x Kelvin temperature).
 - Often ADC quantization and/or background noises lifts this to numbers like -150 dBm/Hz , or “noise figure” in dB increases this level
 - Unrelated radio noises can “color” the noise (must measure $S_{noise}(f)$) and then the channel model with noise-whitening receiver is $H(f) \leftrightarrow S_{noise}^{-1/2}(f) \cdot H(f)$.



Ideal antennas

Ideal isotropic (monopole)

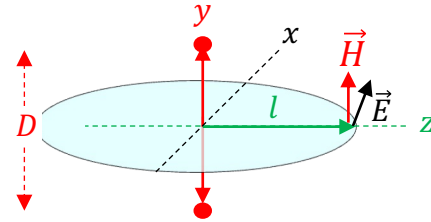


$$\vec{E} = E_0 \cdot \frac{e^{-j(\omega \cdot t - \beta \cdot l)}}{\sqrt{4\pi \cdot l^2}}$$

- Isotropic baseband equivalent

$$\varphi(\omega) = E_0 \cdot \frac{e^{+j\omega \cdot l / (\ell_0 \cdot c)}}{2 \cdot (\ell / \ell_0) \cdot \sqrt{\pi}}$$

- Z_0 free space = $\sqrt{\mu_0 / \epsilon_0} = 377 \Omega$



Dipole planar slice
wire vertical to plane

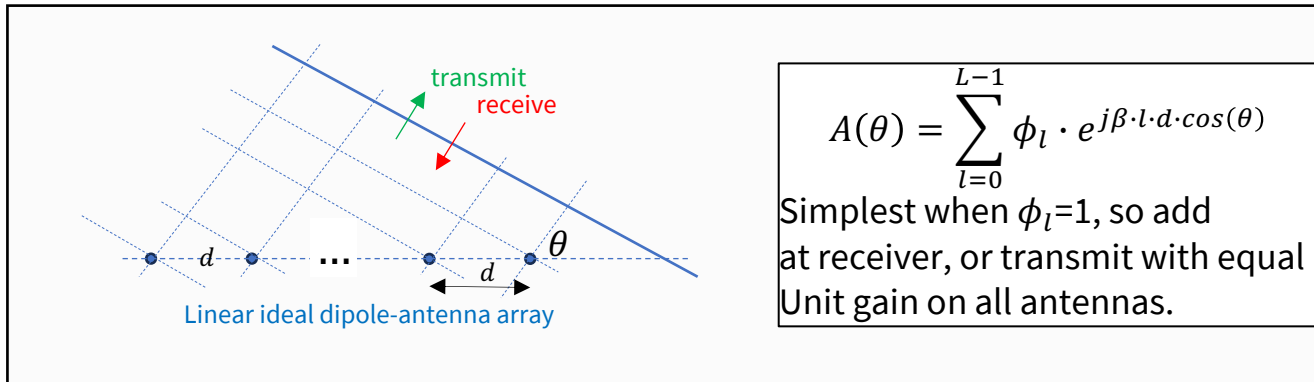
- Dipole planar baseband equivalent
 - Has an unnormalized basis function, and
 - Is typically fed with voltage in middle.
 - A **cross-dipole** supports 2 polarizations, 2nd in vertical disk, so directional

$$\varphi(\omega) = E_{0,dipole} \cdot \frac{e^{+j\omega \cdot l / (\ell_0 \cdot c)}}{2 \cdot (\ell / \ell_0) \cdot \sqrt{\pi}}$$

- Z_0 dipole = $377 / 6\pi = 73 \Omega$
 - Whence, 75 ohm often used in cable connects.



Antenna Arrays

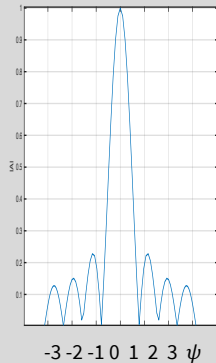


- For receiver, the inter-antenna delays allow multiple looks.
 - Noise is uncorrelated if antenna spacing exceeds $\lambda/2$
 - Largest amplitude is L when $\theta = \pi/2$ with unit gains
- For transmitter, the amplitudes can be set to direct energy in any θ .
- Arrays allow transmitter and receiver to point at one another.



Equal-gain array patterns with L

L=8



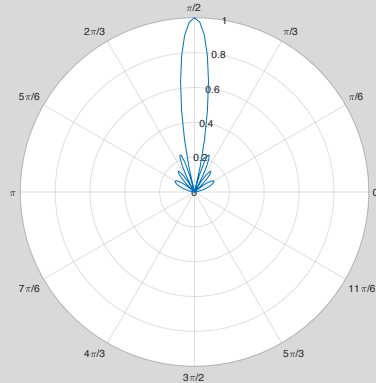
- Equal gains $\alpha_l = 1$

$$|A(\theta)| = \left| \frac{\sin(L \cdot \psi/2)}{L \cdot \sin(\psi/2)} \right|$$

$$\psi \triangleq \beta \cdot d \cdot \cos(\theta)$$

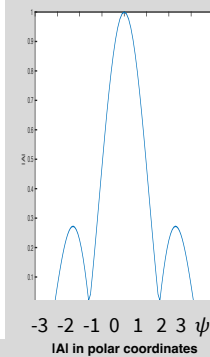
beamform (xmit)
or
beamsteer (rcvr)

IAI in polar coordinates

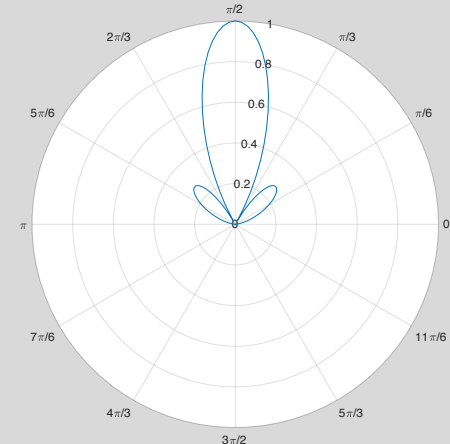


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L=4



IAI in polar coordinates



S4C: 7

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MIMO Beam Forming and Steering

- Each path has $H_{c,k} \cdot \delta(t - \tau_k)$.
- **MIMO** beamform has a linear combination of different symbol-dimensions/antenna.

$$\underbrace{A_{xmit}}_{L_x \times L_x} = \begin{bmatrix} \mathbf{a}_0 \\ \mathbf{a}_1 \\ \vdots \\ \mathbf{a}_{L-1} \end{bmatrix} \quad \text{Each row can steer in its own direction}$$

- Similarly, the receiver can linearly combine (beam steer) $L_x \times L_y$ A_{rcvr} .

- Then

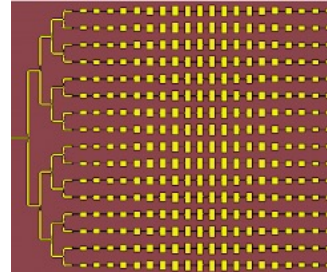
$$H_k = A_{rcvr,k} \cdot H_{c,k} \cdot A_{xmit,k}$$

- Reflections are good – “rich scattering.”



2D Antenna Array

- Usually a rectangular array:



$$A(\theta, \phi) = \sum_{\ell} \mathbf{a}_{\ell} \cdot e^{j \cdot \beta \cdot \mathbf{d}_{\ell} \cdot \mathbf{r}_0} \quad \mathbf{r}_0 = \begin{bmatrix} \cos(\phi) \\ \sin(\phi) \cdot \sin(\theta) \\ \sin(\phi) \cdot \cos(\theta) \end{bmatrix} \quad \text{spherical coordinates}$$

$$|A(\theta, \phi)| = \left| \frac{\sin(L_x \cdot \psi_x / 2)}{L_x \cdot \sin(\psi_x / 2)} \right| \cdot \left| \frac{\sin(L_y \cdot \psi_y / 2)}{L_y \cdot \sin(\psi_y / 2)} \right|$$

- Designs adapt array coefficients to create many beam-form or beam-steer possibilities, see Chapters 4 and 5, and EE379B





End Supplementary Lecture 4C